

Preparation of ethyleneamines

The present invention relates to a process for the preparation of ethyleneamines, in particular diethylenetriamine (DETA), piperazine (PIP) and/or triethylenetetramine (TETA), by continuous reaction of ethylenediamine (EDA) in the presence of a heterogeneous catalyst.

Ethyleneamines are used as solvents, stabilizers, for the synthesis of chelating agents, synthetic resins, medicaments, inhibitors and interface-active substances.

In particular, diethylenetriamine (bis(2-aminoethyl)amine; DETA) is used as solvent for dyes and is a starting material for the preparation of ion exchangers, pesticides, antioxidants, corrosion inhibitors, complexing agents, textile auxiliaries and absorption agents for (acidic) gases.

The ethylenediamine ($\text{H}_2\text{N}-\text{CH}_2-\text{CH}_2-\text{NH}_2$; EDA) required as starting material can be prepared by known processes, for example by reaction of monoethanolamine (MEOA) with ammonia.

Numerous processes are described in the literature for the preparation of ethyleneamines.

According to the prior art, ethyleneamines such as DETA are prepared from monoethanolamine (MEOA) and ammonia mostly in fixed-bed reactors, where the catalysts comprise, as active component, for example nickel, cobalt, copper, noble metals such as Re, Ru, Rh, Pt, Pd, or combinations thereof. Support material may, for example, be Al_2O_3 , SiO_2 or ZrO_2 or combinations of these and other oxides. To maintain the catalyst activity, it is in most cases necessary to introduce small amounts of hydrogen (e.g. about 0.001% by weight, based on the amount of feed).

The main product which arises in the process is EDA, and by-products which arise are DETA, piperazine (PIP) and higher ethyleneamines, i.e. ethyleneamines with a boiling point higher than DETA (at the same pressure), and other compounds, such as, for example, aminoethylethanolamine (AEEA).

Since DETA in particular is demanded on the market in relatively large amounts as well as the main product EDA, it is desirable to increase the selectivity of DETA compared to the selectivity obtained in a simple pass in the fixed-bed reactor. The selectivity of EDA and DETA can be controlled within certain limits by the molar ratio of ammonia to MEOA. A high ammonia excess favors the formation of EDA, particularly at a low

MEOA conversion. At a low ammonia excess and a relatively large MEOA conversion, the selectivity of DETA, but also of the other by-products is increased.

5 It is also possible to return some of the EDA, following concentration of the reaction product, to the reactor, in order to increase the DETA selectivity. The formation of the other by-products, in particular AEEA, can, however, not thereby be avoided.

10 EP-A2-197 611 (Union Carbide Corp.) describes a process for the preparation of polyalkylenepolyamines by using two reactors connected in series.

In the first reactor, the amination of MEOA with ammonia takes place over transition metal catalysts (Ni, Re, support).

15 The reactor product is sent via a second reactor, which is likewise charged with a transition metal catalyst or with a phosphate catalyst. To control the product distribution and to increase the selectivity with respect to the linear ethyleneamines, ethylenediamine which originates from the work-up of the reaction product of the second reactor and also comprises MEOA and H₂O is introduced before the second reactor.

20 A disadvantage of this process is that AEEA preferentially further reacts to give piperazine and not to give DETA, and additional amounts of AEEA are formed as a result of the reaction of EDA with MEOA.

25 The synthesis of DETA can take place by known methods also by reacting EDA in a fixed-bed reactor, where the by-product produced is mainly PIP (cf. e.g. US 5,410,086 (Burgess), GB-A-1,508,460 (BASF AG) and WO-A1-03/010125 (Akzo Nobel)).

30 At a conversion of, for example, about 30%, a DETA selectivity of about 70% can be achieved. If pure EDA is used as starting material, no AEEA is formed as by-product. The formation of higher ethyleneamines is largely avoided by the partial conversion procedure.

35 Due to the unfavorable position of the chemical equilibria, however, more PIP would be formed at a higher conversion. Furthermore, due to the formation of ammonia during the conversion of EDA to DETA ($2 \text{ EDA} \rightarrow \text{DETA} + \text{NH}_3$), the back reaction of DETA with ammonia to give EDA is also increasingly gaining in importance.

40 The partial conversion procedure leads to high circulation streams of EDA (recycle) and thus to increased energy consumption, particularly in the EDA purification column.

BASF's German patent application No. 10335991.5 of August 1, 2003 relates to a process for the preparation of ethyleneamines by reacting monoethanolamine (MEOA) with ammonia in the presence of a catalyst in a reactor (1) and separating the resulting reaction product, where ethylenediamine (EDA) obtained during the separation is
5 reacted in a separate reactor (2) in the presence of a catalyst to give diethylenetriamine (DETA), and the resulting reaction product is passed to the separation of the reaction product resulting from reactor 1.

For the addition of alcohols onto olefins to give corresponding ethers [e.g. MTBE
10 (methyltertiary-butyl ether) and TAME (tertiary-amyl methyl ether)] there are processes known in the literature which are carried out in a reaction column. The processes, also referred to as reactive distillation, are described in detail, for example, in the textbook "Reactive Distillation", edited by K. Sundmacher and A. Kienle, Verlag Wiley-VCH
15 (2003).

Applications of reactive distillation also exist in the fields of esterifications, saponifications and transesterifications, preparation and saponification of acetals, preparation of alkoxylates, aldol condensations, alkylations, hydrolysis of epoxides, hydration of olefins, isomerizations and hydrogenations.

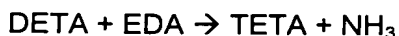
20 It is an object of the present invention to find an improved economical process for the selective preparation of ethyleneamines, including, in particular, diethylenetriamine (DETA), in high yield and space-time yield (STY).

25 [Space-time yields are given in 'product quantity/(catalyst volume • time)' (kg/(l_{cat.} • h)) and/or 'product quantity/(reactor volume • time)' (kg/(l_{reactor} • h)).

We have found that this object is achieved by a process for the preparation of ethyleneamines by continuous reaction of ethylenediamine (EDA) in the presence of a
30 heterogeneous catalyst, which comprises carrying out the reaction in a reaction column.

The ethyleneamines are, in particular, diethylenetriamine (DETA), piperazine (PIP) and/or triethylenetetramine (TETA).

35 The reaction proceeds, then, for example, in accordance with the following equations:



According to the invention, it has been recognized that the disadvantages of the processes of the prior art are avoided when the synthesis of ethyleneamines, in particular DETA, is carried out by continually reacting EDA in a reaction column
5 (reactive distillation). The continuous stripping of DETA and/or TETA from the column below the reaction zone (via the bottom and/or via a side take-off) can largely suppress secondary reactions and thereby permit a procedure with a high conversion and even complete conversion of EDA.

10 By continuously removing ammonia from the column (preferably at the top of the column, also as a mixture with components with lower boiling points than DETA), the back reaction of DETA to EDA is largely suppressed, thus accelerating the formation of DETA. The reaction can thus be carried out at other pressures, advantageously lower pressures, than in the optimum pressure range when using a conventional fixed-bed
15 reactor (tubular reactor with catalyst fixed bed).

The absolute pressure in the column is preferably in the range from > 0 to 20 bar, for example in the range from 1 to 20 bar, in particular 5 to 10 bar.

20 The temperature in the section of the column in which the reaction of EDA to ethyleneamines takes place (reaction zone) is preferably in the range from 100 to 200°C, in particular 140 to 160°C.

The number of theoretical plates in the column is preferably in the range from 5 to 100
25 in total, more preferably 10 to 20.

The number of theoretical plates in the reaction zone is preferably in the range from 1 to 30, in particular 1 to 20, in particular 1 to 10, for example 5 to 10.

30 The number of theoretical plates in the enriching section above the reaction zone is preferably in the range from 0 to 30, in particular 1 to 30, more particularly 1 to 15, in particular 1 to 5.

The number of theoretical plates in the stripping section below the reaction zone is
35 preferably in the range from 0 to 40, particularly 5 to 30, in particular 10 to 20.

The addition of EDA to the column can take place below the reaction zone in liquid form or in gaseous form.

The addition of EDA to the column can also take place in liquid form above the reaction
40 zone.

In the process according to the invention, both pure EDA, e.g. in a purity of > 98% by weight, in particular > 99% by weight, and also EDA which comprises piperazine (PIP), e.g. > 0 to 25% by weight of PIP, and/or other ethyleneamines, can be fed into the column.

5

It is also possible to use the EDA crude product from a reaction of MEOA with ammonia following partial or complete removal of ammonia and water.

The reaction is particularly preferably carried out in the presence of hydrogen, in particular in the presence of from 0.0001 to 1% by weight, preferably 0.001 to 0.01% by weight, of hydrogen, based on the feed amount of EDA.

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The addition of hydrogen to the column preferably takes place below the reaction zone.

A mixture of ammonia, other components with a boiling point lower than DETA (at the same pressure) (low-boiling components) and optionally hydrogen is preferably removed via the top of the column.

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The mixture removed via the top of the column can also comprise partial amounts of unreacted EDA.

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The mixture removed overhead can also be partially condensed and, during this, ammonia and optionally hydrogen are removed predominantly in gaseous form (evaporated off) and the liquefied fraction can be fed to the column as reflux.

The weight ratio of the amount of reflux of the column (column reflux amount) to the amount of feed to the column is here preferably in the range from 0.1 to 30, particularly preferably 0.5 to 10, in particular 0.5 to 2..

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A mixture of DETA, piperazine (PIP), TETA and other components with a boiling point higher than that of DETA (at the same pressure) (high-boiling components) is preferably removed via the bottom of the column.

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The mixture removed via the bottom of the column may also comprise partial amounts of unreacted EDA or the total amount of unreacted EDA.

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In one particular embodiment, the column below the reaction zone is subdivided by a side take-off.

Unreacted EDA, PIP or mixtures thereof are preferably removed via the side take-off.

The product removed via the side take-off may also comprise DETA.

The product produced via the side take-off is removed in liquid form or in gaseous form.

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In the reaction zone, the catalyst used is preferably a catalyst comprising Ni, Co, Cu, Ru, Re, Rh, Pd and/or Pt or a shape-selective zeolite catalyst or a phosphate catalyst.

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The metal or metals of the transition metal catalyst, which preferably include Ru, Re, Rh, Pd and/or Pt, have preferably been applied to an oxidic support material (e.g. Al_2O_3 , TiO_2 , ZrO_2 , SiO_2) or to a zeolite or active carbon support material.

15

In a preferred embodiment, the catalyst used in the reaction zone is a catalyst comprising Pd and zirconium dioxide support material.

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The total metal content of the supported transition metal catalysts is preferably in the range from > 0% to 80% by weight, particularly 0.1% to 70% by weight, more particularly 5% to 60% by weight, more particularly 10% to 50% by weight, all percentages being based on the weight of the support material.

25

In the case of supported noble metal catalysts, which are preferred, the total noble metal content is in particular in the range from > 0% to 20% by weight, particularly 0.1% to 10% by weight, very particularly 0.2% to 5% by weight, more particularly 0.3% to 2% by weight, all percentages being based on the weight of the support material.

30

The heterogeneous catalysts can be accommodated in the form of fixed catalyst beds within the column or in separate containers outside the column. They can also be used as loose beds, e.g. as a loose bed in a distillation packing, be shaped to give dumped packings or moldings, for example pressed to give Raschig rings, incorporated into filter fabric and shaped to give bales or column packings, applied to distillation packings (coating) or be used in the form of a suspension in the column, here preferably in the form of a suspension on column trays.

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In processes with heterogeneously catalyzed reactive distillations, the bales technology developed by CDTech can advantageously be used.

Further technologies are special tray constructions with packed or suspended catalysts.

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Multichannel packings or cross channel packings (see e.g. WO-A-03/047747) permit

simple insertion and removal of catalysts which are in particulate form (e.g. spheres, pellets, tablets) with low mechanical stress of the catalyst.

- 5 An important point for reactive distillation is the provision of the residence time required for the course of the reaction. It is necessary to increase the residence time of the liquid in the column in a targeted manner compared with a nonreactive distillation. Special designs of column internals, for example tray columns with bubblecap trays with considerably increased fill level, high residence times in the downcomers of tray columns and/or also separately arranged external delay-time containers are used.
- 10 Obstructive packings offer the possibility of increasing the residence time of the liquid by approximately a factor of 3 compared with columns packed with dumped or arranged packing.

- 15 The design of the reaction column (number of plates in the column sections enriching section, stripping section and reaction zone, reflux ratio, etc.) can be undertaken by the person skilled in the art in accordance with methods with which he is familiar.

Reaction columns are described, for example, in the literature in:

- 20 "Reactive distillation of nonideal multicomponent mixtures", U. Hoffmann, K. Sundmacher, March 1994, Trondheim/Norway,
 "Prozesse der Reaktivdestillation" [Processes of reactive distillation], J. Stichlmair, T. Frey, Chem. Ing. Tech. 70 (1998) 12, pages 1507-1516,
 "Thermodynamische Grundlagen der Reaktivdestillation" [Thermodynamic principles of
 25 reactive distillation], T. Frey, J. Stichlmair, Chem. Ing. Tech. 70 (1998) 11, pages 1373-1381,
 WO-A-97/16243 dated 9.5.97,
 DD-Patent 100701 dated 5.10.73,
 US 4,267,396 dated 12.5.81,
- 30 "Reaktionen in Destillationskolonnen" [Reactions in distillation columns], G. Kaibel, H.-H. Mayer, B. Seid, Chem. Ing. Tech. 50 (1978) 8, pages 586-592, and literature cited therein,
 DE-C2-27 14 590 dated 16.8.84,
 EP-B-40724 dated 25.5.83,
- 35 EP-B-40723 dated 6.7.83,
 DE-C1-37 01 268 dated 14.4.88,
 DE-C1-34 13 212 dated 12.9.85,
 "Production of potassium tert-butoxide by azeotropic reaction distillation", Wang Huachun, Petrochem. Eng. 26 (1997) 11,
- 40 "Design aspects for reactive distillation", J. Fair, Chem. Eng. 10 (1998), pages 158-162,

EP-B1-461 855 dated 09.08.95,

"Consider reactive distillation", J. DeGarmo, V. Parulekar, V. Pinjala, Chem. Eng. Prog. 3 (1992),

EP-B1-402 019 dated 28.6.95,

- 5 "La distillation réactive", P. Mikitenko, Pétrole et Techniques 329 (1986), pages 34-38,
"Geometry and efficiency of reactive distillation bale packing", H. Subawalla,
J. González, A. Seibert, J. Fair, Ind. Eng. Chem. Res. 36 (1997), pages 3821-3832,
"La distillation réactive", D. Cieutat, Pétrole et Techniques 350 (1989),
"Preparation of tert-amyl alcohol in a reactive distillation column", J. González,
10 H. Subawalla, J. Fair, Ind. Eng. Chem. Res. 36 (1997), pages 3845-3853,
"More uses for catalytic distillation", G. Podrebarac, G. Rempel, Chem. Tech. 5 (1997),
pages 37-45,
"Advances in process technology through catalytic distillation", G. Gildert, K. Rock,
T. McGuirk, CDTech, pages 103-113,
15 WO-A1-03/047747 dated 12.06.03 (BASF AG), and
WO-A1-97/35834.

In a preferred embodiment, the process of the present invention is carried out as described in WO-A1-03/047747 in a column for carrying out reactive distillations in the
20 presence of a heterogeneous particulate catalyst having an ordered packing or random packings which form intermediate spaces in the column interior, wherein the column has first and second part regions which are arranged in alternation and which differ by the specific surface area of the ordered packing or random packings in such a manner that in the first part regions the quotient of hydraulic diameter for the gas stream
25 through the ordered packing or random packings and equivalent diameter of the catalyst particles is in the range from 2 to 20, preferably in the range from 5 to 10, with the catalyst particles being introduced into the intermediate spaces, distributed and discharged loose under the action of gravity and in the second part regions the quotient of the hydraulic diameter for the gas stream through the ordered packing or random
30 packings and equivalent diameter of the catalyst particles is less than 1 and no catalyst particles are introduced into the second part regions. Preferably the column is operated with respect to its gas and/or liquid loadings in such a manner that a maximum of from 50% to 95% and preferably from 70% to 80% of the flooding limit loading is reached. Cf. loc. cit., claims 9 and 10.

35 The work-up of the product streams produced in the process according to the invention, which primarily comprise the particularly desired DETA, but also triethylenetriamine (TETA), PIP and unreacted EDA, can take place in accordance with the distillation process known to the person skilled in the art. (compare e.g. PEP Report
40 No. 138, "Alkyl Amines", SRI International, 03/1981, pages 81-99, 117).

The distillation columns required for the distillative isolation of the individual pure products, primarily of the particularly desired DETA, can be designed by the person skilled in the art using methods with which he is familiar (e.g. number of plates, reflux ratio, etc.).

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The procedure with a side take-off in the stripping section below the reaction zone of the reaction column offers particular advantages during the further work-up for isolating the individual pure products.

- 10 The side take-off stream, consisting primarily of PIP, unreacted EDA or mixtures thereof, comprises only small amounts of DETA and high-boiling components, in particular in the case of the gaseous removal of the side take-off stream. It can therefore be fed directly within the work-up section, separately from the bottom take-off stream of the reaction column, to the place where the purification of EDA and PIP is
- 15 carried out, instead of firstly passing through the removal of the low-boiling components from DETA and high-boiling components.

- Partial amounts of the side stream can also be returned to the reaction column itself. This is particularly advantageous when the side stream comprises primarily EDA and
- 20 little or no PIP.

- The bottom take-off stream of the reaction column in this procedure comprises fewer low-boiling components (EDA and PIP), thus relieving the pressure on the column for removing the low-boiling components from DETA and high-boiling components.

25

- If the reactive distillation is carried out at low pressures, for example 1 to 3 bar, it is also possible to obtain the bottom take-off stream at bottom temperatures of from about 200 to 240°C free from EDA and PIP. The bottom take-off stream can then optionally be passed to the work-up section at the place where the purification of DETA is carried
- 30 out, instead of firstly passing through the separation of the low-boiling components from DETA and high-boiling components.

- The process of the present invention makes it possible to produce DETA at a selectivity of > 18%, especially > 20% and more particularly > 22%, all percentages being based
- 35 on EDA, coupled with an EDA conversion of > 30%, especially > 40% and more particularly > 50%.

Examples

Example A

- 5 Figure 1 in Annex 1 shows a version of the process according to the invention in which pure EDA or an EDA/PIP mixture is fed, together with hydrogen, to the reaction column continuously below the catalytic packing, and a mixture comprising DETA, unreacted EDA, PIP, TETA and high-boiling components (SS, i.e. components with a boiling point higher than DETA) is obtained via the bottom. Ammonia, hydrogen and low-boiling components (LS, i.e. components with a boiling point lower than DETA) are separated off overhead.

Example B

- 15 Figure 2 in Annex 2 shows a version of the process according to the invention in which pure EDA or an EDA/PIP mixture, together with hydrogen, is passed to the reaction column continuously below the catalytic packing, and a mixture comprising DETA, TETA and high-boiling components (SS, i.e. components with a boiling point higher than DETA) is obtained via the bottom. Ammonia, hydrogen and low-boiling components (LS, i.e. components with a boiling point lower than DETA) are removed overhead.

In a side take-off in the stripping section below the reaction zone of the reaction column, PIP, optionally as a mixture with EDA, is separated off.

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Examples 1 to 4

- The catalyst was prepared using zirconium dioxide extrudates 3.2 mm in diameter and 1-2 cm in length.
- 30 2700 g of the support were drenched with 770.0 ml (= 92% of H₂O uptake) of an aqueous palladium nitrate solution, resulting in a calculated palladium loading of 0.9% by weight of palladium. The drenching was carried out repeatedly. This was followed by drying in a drying cabinet at 120°C (heating to 120°C took 1 h) for 6 h and calcination in a muffle furnace at 450°C (heating to 450°C took 2 h) for 2 h.

35

The reactions of examples 1 to 4 were all carried out at an absolute pressure of 5 bar. Hydrogen was fed into the column at below the catalytic layer at a rate of 6 l/h.

- 40 Examples 1 and 2 were carried out after 755 g of the prepared catalyst had been filled into a 55 mm diameter laboratory column containing an ordered packing as recited in

claim 9 of patent application WO-A1-03//047747 and the related description.

The number of theoretical plates below the catalyst bed was 6. The catalytic packing had 3.5 theoretical plates. The number of theoretical plates above the catalyst bed was 1.

5

Example 1

Liquid EDA was supplied at room temperature above the catalytic layer at a rate of 400 g/h. Reflux was set to 800 g/h. The base of column temperature in steady-state operation was 186°C.

10

The bottom product of the column had a composition (in % by weight) of 65% EDA, 9.7% DETA and 16% piperazine. The other components were high boilers. This amounted to a DETA selectivity of 25% coupled with an EDA conversion of 41%.

15

Example 2

Liquid EDA was supplied at room temperature below the catalytic layer at a rate of 400 g/h. Reflux was set to 400 g/h. The base of column temperature in steady-state operation was 183°C.

20 The bottom product of the column had a composition (in % by weight) of 74.6% EDA, 6.1% DETA and 13.2% piperazine. The other components were high boilers. This amounted to a DETA selectivity of 21.7% coupled with an EDA conversion of 30.6%.

25 Example 3 was carried out after 934 g of the prepared catalyst had been filled into a 55 mm diameter laboratory column containing an ordered packing as recited in claim 9 of patent application WO-A1-03//047747 and the related description.

30 The number of theoretical plates below the catalyst bed was 15. The catalytic packing had 10 theoretical plates. The number of theoretical plates above the catalyst bed was 10.

Example 3

35 Liquid EDA was supplied at room temperature above the catalytic layer at a rate of 100 g/h. Reflux was set to 800 g/h. The base of column temperature in steady-state operation was 162°C.

The bottom product of the column had a composition (in % by weight) of 55% EDA, 12% DETA and 21% piperazine. The other components were high boilers. This amounted to a DETA selectivity of 21% coupled with an EDA conversion of 55%.